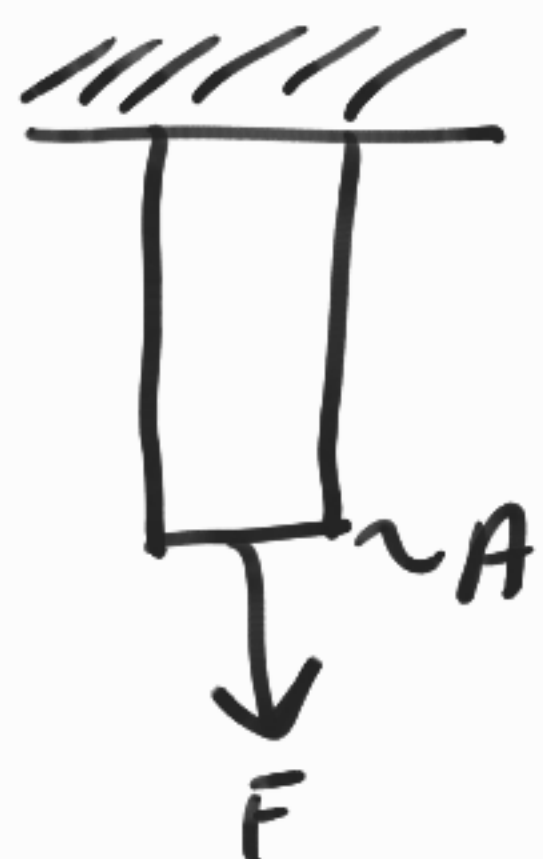
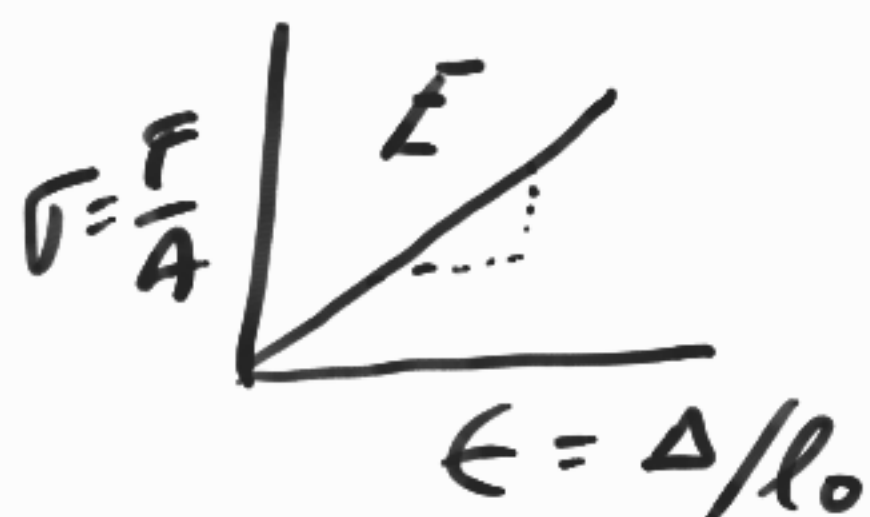


5. CONSTITUTIVE LAWS

THESE ARE THE EQUATIONS THAT DEFINE HOW STRESS IS RELATED TO STRAIN. FOR EXAMPLE (4.3)



$$\sigma = \frac{F}{A}$$
$$\epsilon = \Delta / l_0$$


$$\sigma = E \epsilon$$

is a constit. law

INCOMPRESSIBLE - A MATERIAL THAT DOES NOT CHANGE VOLUME

COMPRESSIBLE - CAN CHANGE VOLUME (SPONGE)

ELASTIC - A DEFORMATION THAT IS FULLY REVERSED WHEN FORCES ARE REMOVED (RUBBER BAND SNAPS BACK)

5.1 LINEAR ELASTIC: STRESS $\underline{\underline{\sigma}}$ IS LINEARLY RELATE

TO $\underline{\underline{\epsilon}}$, AS ABOVE. BUT IF WE DO NOT ASSUME 1D, OR ISOTROPIC, 4.3 GENERALIZES TO

$$\underline{\underline{\sigma}} = \underline{\underline{C}} \underline{\underline{\epsilon}} \quad (5.1)$$

IN COMPONENT FORM

$$\sigma_{ij} = C_{ijkl} \epsilon_{kl} \quad (5.2)$$

WHERE $\underline{\underline{C}}$ IS THE 4TH ORDER STIFFNESS TENSOR.

ISOTROPIC - ISOTROPIC LINEAR ELASTIC SOLIDS ARE
DEFINED BY 2 PARAMETERS ONLY



eg fat, liver

E - Young's Modulus

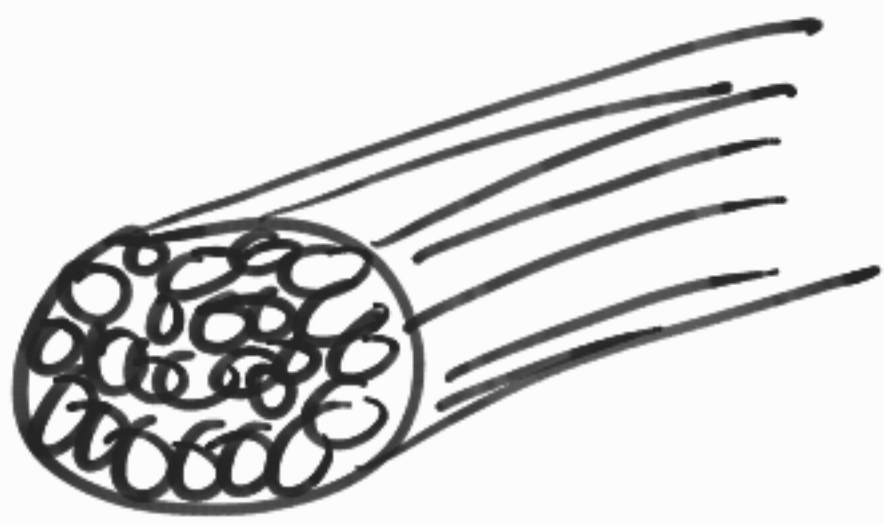
ν - Poisson's Ratio

$$\nu = -\epsilon_t / \epsilon_a \quad \left(\begin{array}{c} \text{transverse} \\ \text{applied} \end{array} \right)$$

$$\sigma_{ij} = \frac{E}{(1+\nu)} \left[\epsilon_{ij} + \frac{\nu}{1-2\nu} \epsilon_{kk} \delta_{ij} \right] \quad \underline{\underline{5.4}}$$

For INCOMPRESSIBLE MATERIALS $\nu = 0.5$

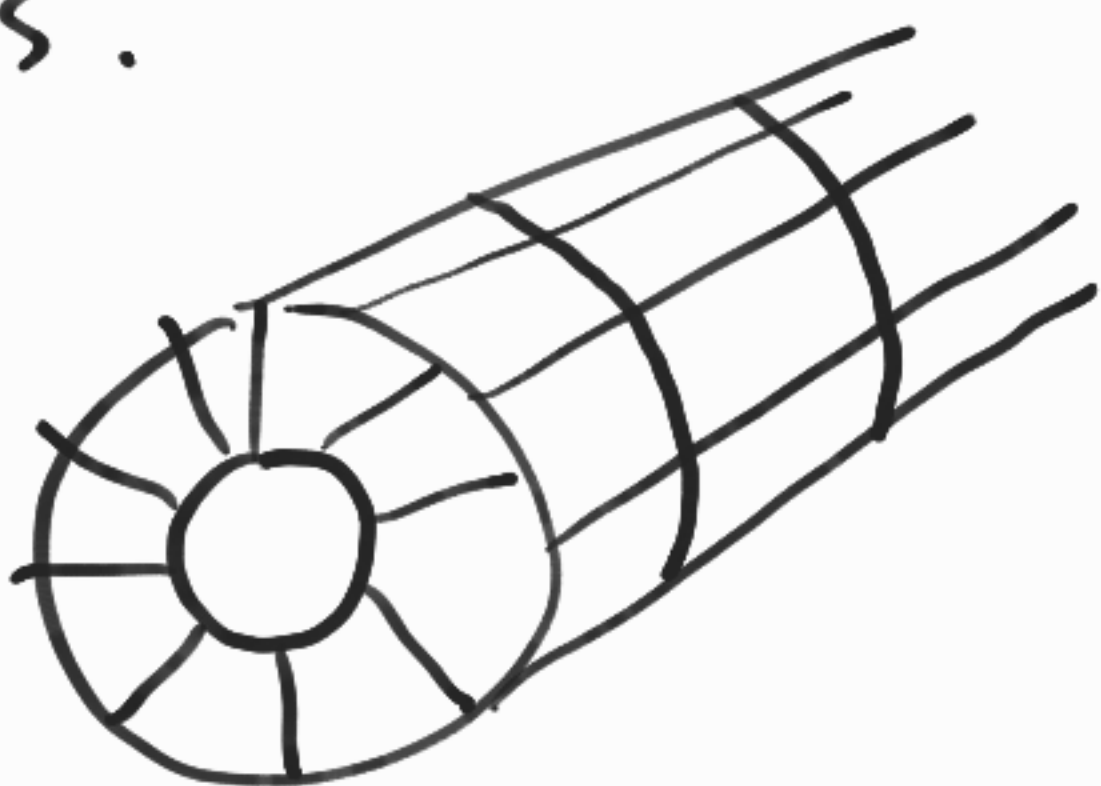
TRANSVERSELY ISOTROPIC - ISOTROPIC EXCEPT IN
ONE DIRECTION. EXAMPLES: tendon, skeletal muscle



DEFINED BY 5 CONSTANTS

$$E_t, \nu_t, E_f, \nu_f, \nu_{tf}$$

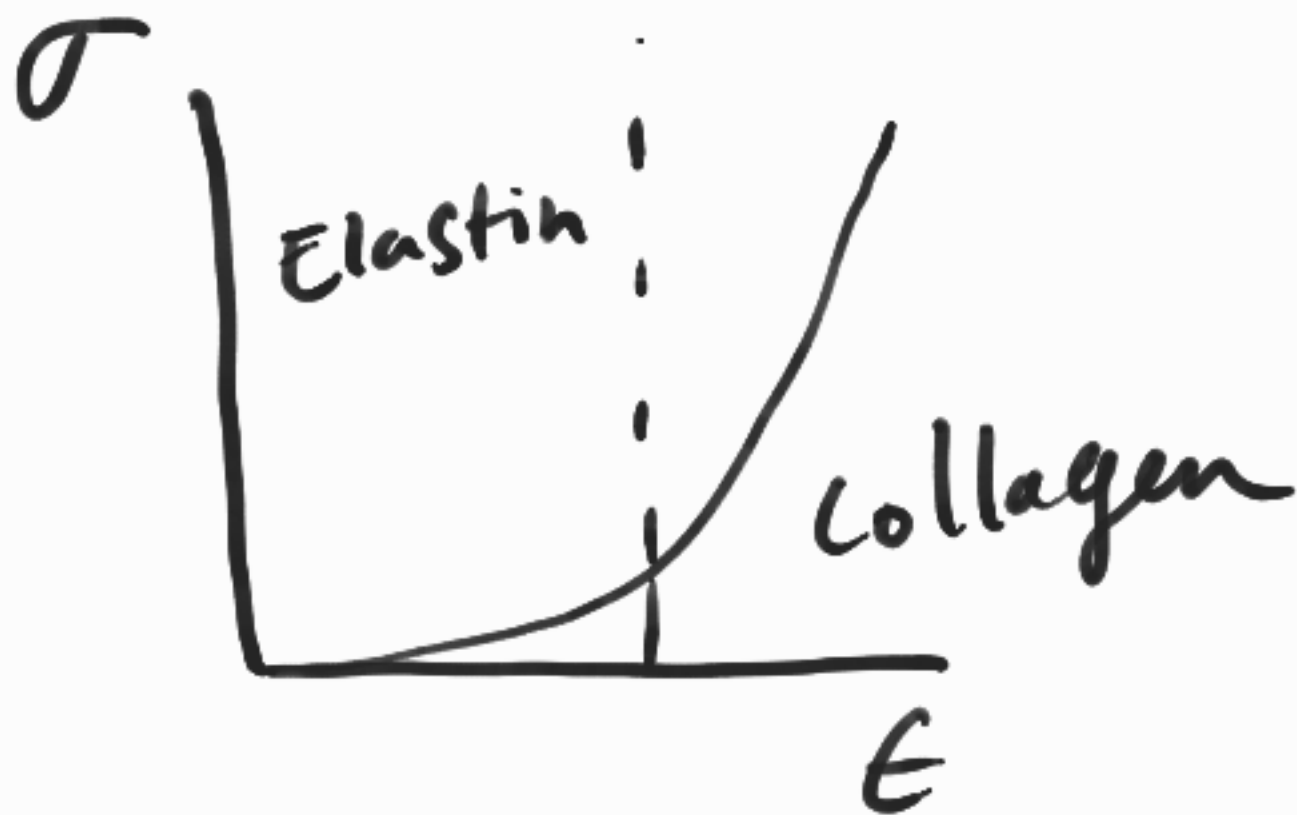
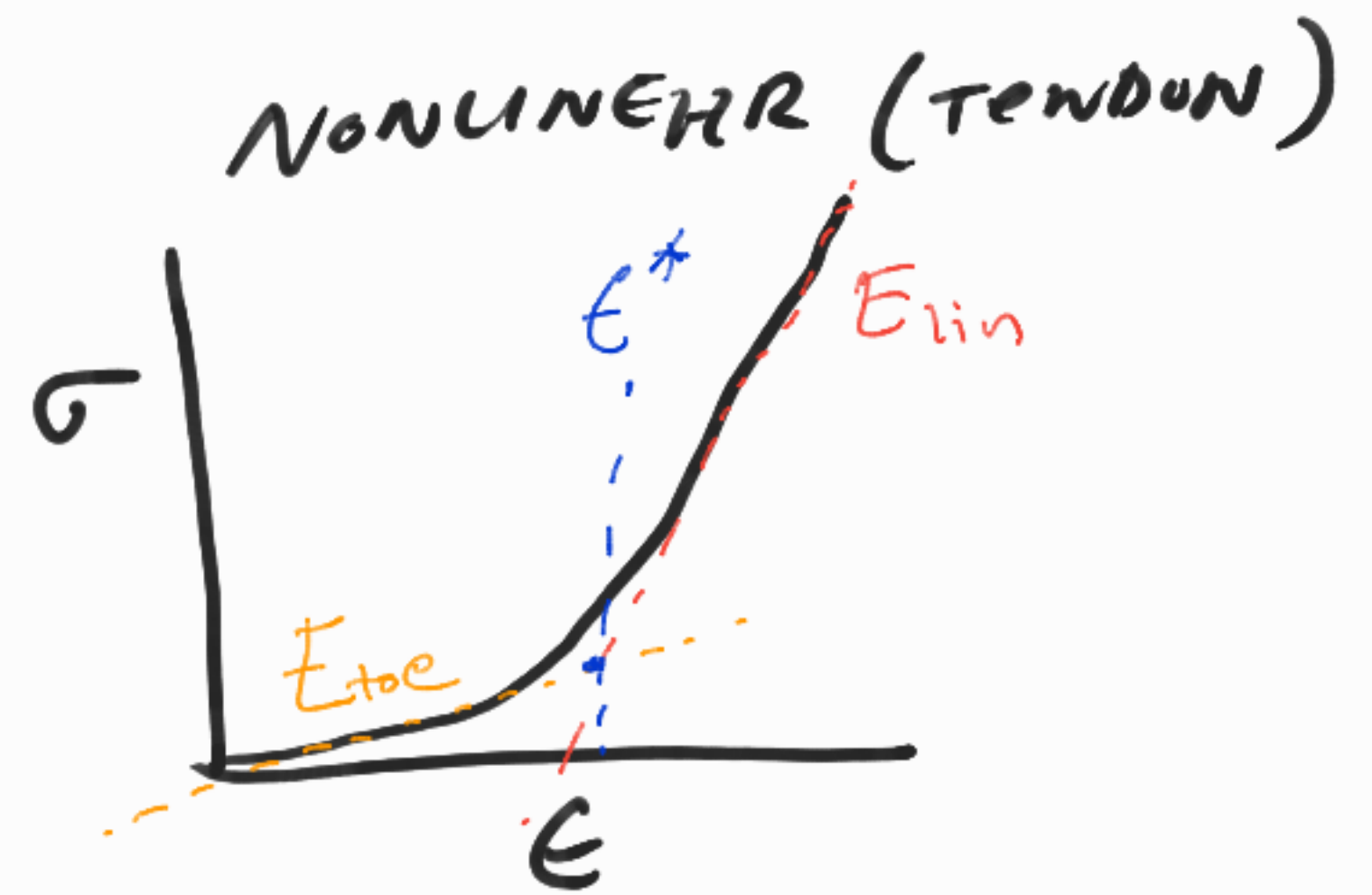
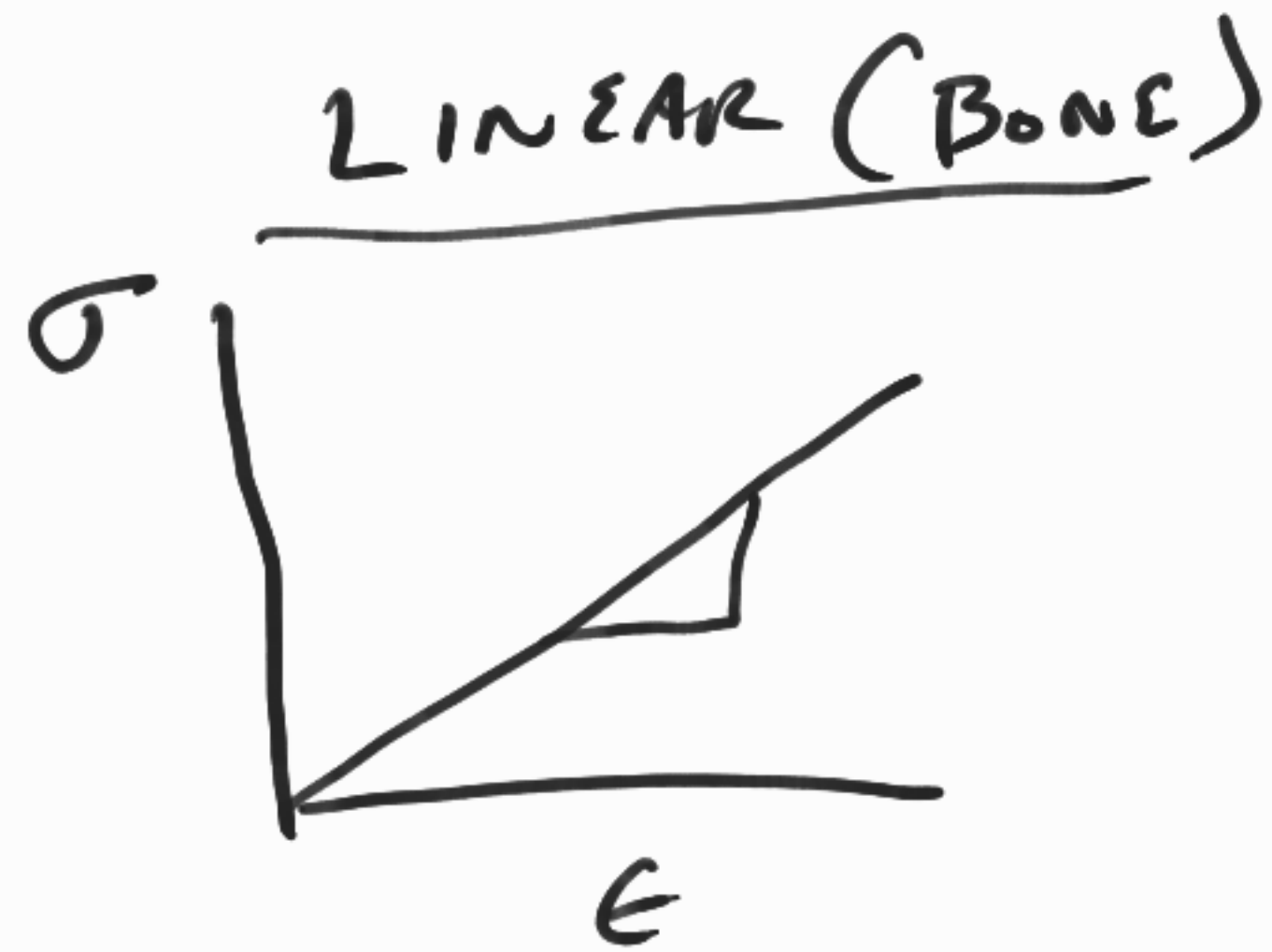
ORTHOTROPIC - PROPERTIES DIFFER ALONG 3 ORTHOGONAL
AXES.



EXAMPLE: ARTERIES

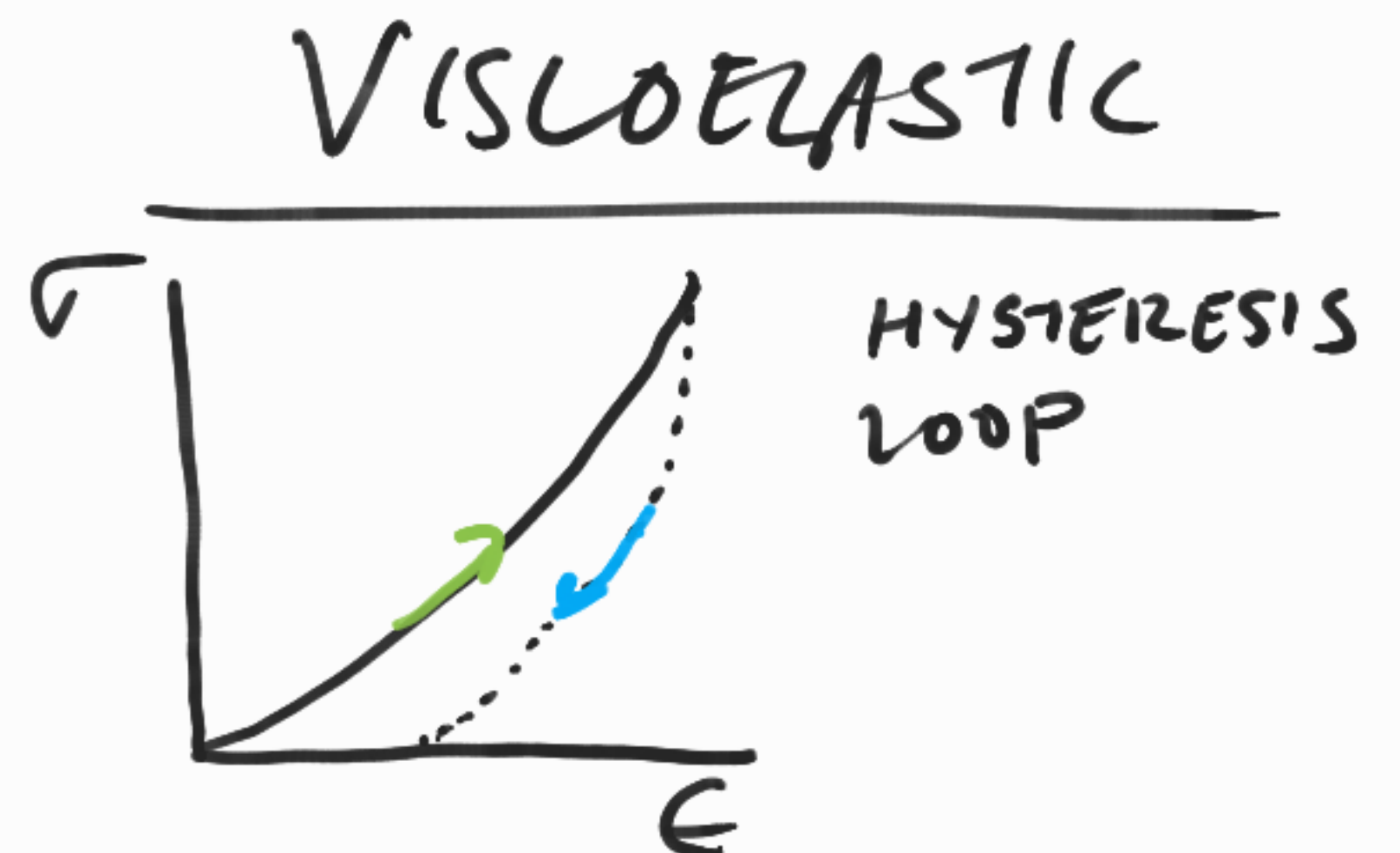
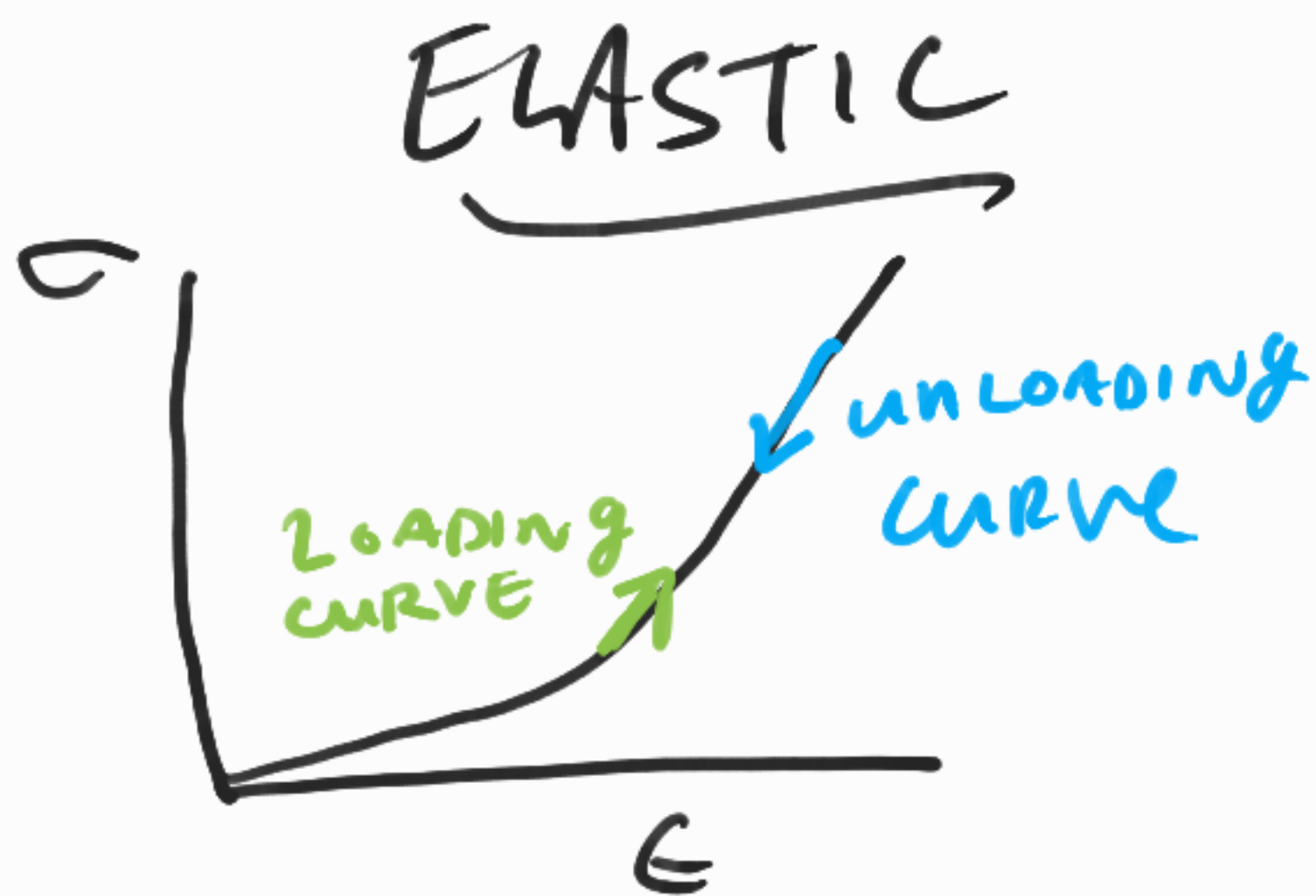
DEFINED BY 9 CONSTANTS.

5.2 NONLINEARITY

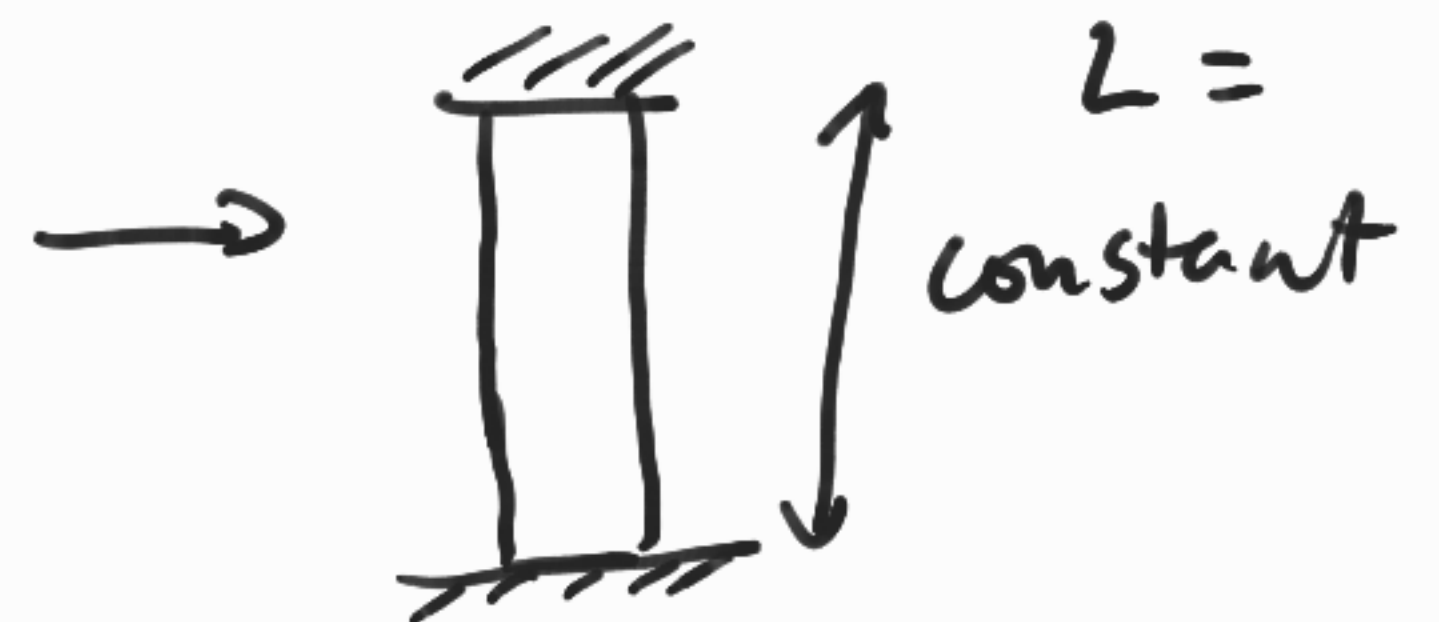
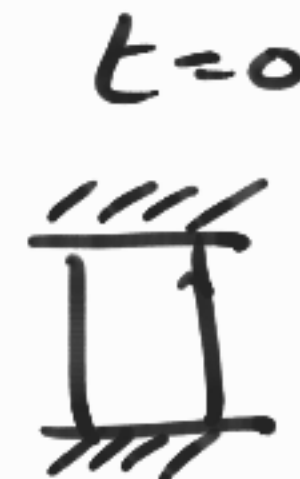


E_{Toe} - Toe region Modulus
 E_{lin} - linear region Modulus
 ϵ^* - transition strain

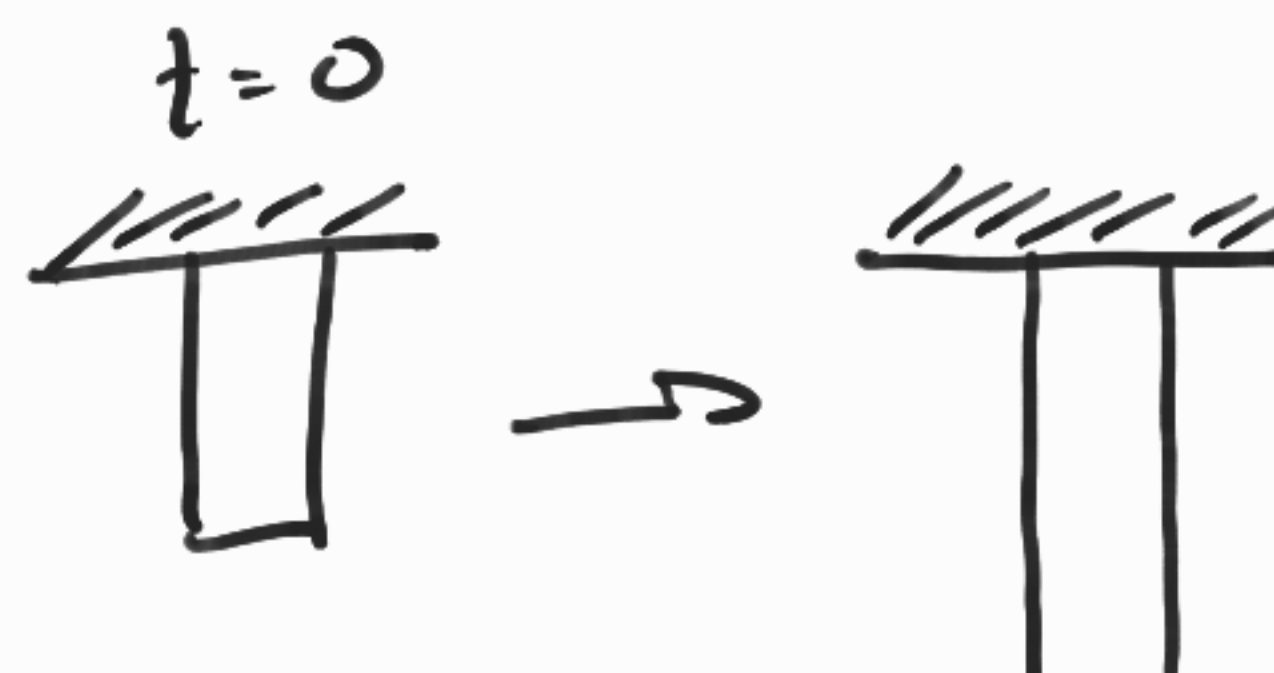
5.3 VISCOELASTICITY

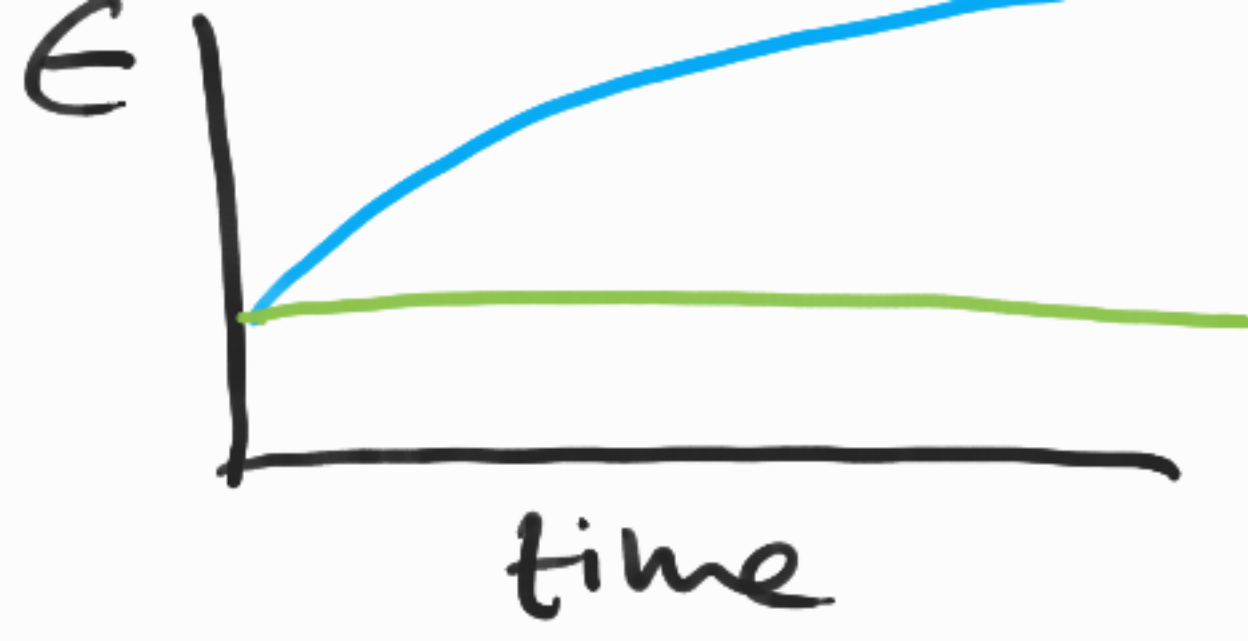



STRESS RELAXATION



Creep

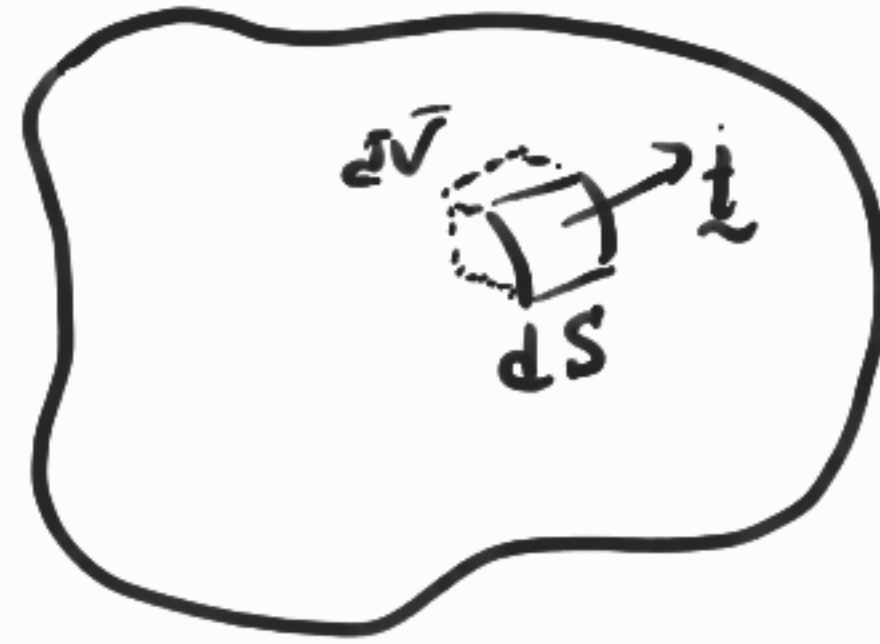




 $F = \text{constant}$

6. EQUATIONS OF MOTION

CONSIDER A BODY WITH SURFACE S AND VOLUME V
SUBJECT TO FORCES ON ITS SURFACE $\underline{t}^{(n)}_{\sim} n=1,2,3,4,\dots$
AND BODY FORCES \underline{f}_{\sim}



WE BEGIN WITH

$$\sum \underline{F}_{\sim} = m \underline{a}_{\sim} = \frac{d}{dt} (m \underline{v}_{\sim}) \quad \underline{\underline{6.1}}$$

WHICH CAN BE REWRITTEN AS

$$\int_S \underline{n}_{\sim} \cdot \underline{\sigma}_{\sim} dS + \int_V \underline{f} dV = \frac{d}{dt} \int_V \underline{v}_{\sim} \rho dV \quad \underline{\underline{6.2}}$$

DIVERGENCE THEOREM SAYS

$$\int_S \underline{n}_{\sim} \cdot \underline{F}_{\sim} dS = \int_V \underline{\nabla}_{\sim} \cdot \underline{F}_{\sim} dV \quad \underline{\underline{6.3}}$$

CAN USE 6.3 TO CONVERT 6.2 TO ALL VOLUME INTEGRALS
(Leibnitz Rule)

$$\int_V \underline{\nabla}_{\sim} \cdot \underline{\sigma}_{\sim} dV + \int_V \underline{f} dV = \frac{d}{dt} (\underline{v}_{\sim} \rho dV) \quad \underline{\underline{6.4}}$$

$$= \int_V \frac{d\rho}{dt} dV + \int_V \rho \frac{\partial}{\partial t} (v_i v_i) dV$$

constant mass

hence

$$\int_V \nabla \cdot \underline{\underline{\sigma}} dV + \int_V \underline{\underline{f}} dV = \int_V \rho \underline{\underline{a}} dV$$

or

$$\boxed{\nabla \cdot \underline{\underline{\sigma}} + \underline{\underline{f}} = \rho \underline{\underline{a}}}$$

6.5

"EQUATIONS OF MOTION"

IN CARTESIAN COMPONENTS,

$$\boxed{\frac{\partial \sigma_{ij}}{\partial x_i} + f_j = \rho a_j}$$

6.6